

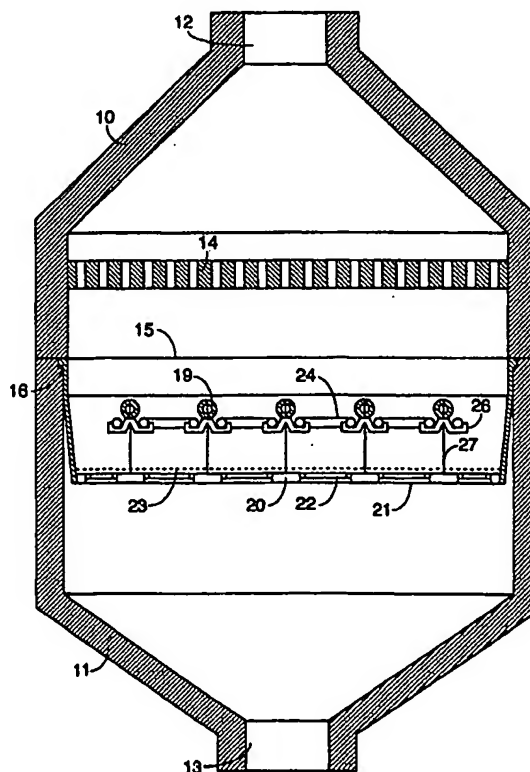


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(21) International Application Number: PCT/GB99/04188 (22) International Filing Date: 10 December 1999 (10.12.99) (30) Priority Data: 9900314.7 8 January 1999 (08.01.99) GB (71) Applicant (for all designated States except US): IMPERIAL CHEMICAL INDUSTRIES PLC [GB/GB]; Imperial Chemical House, Millbank, London SW1P 3JF (GB). (72) Inventor; and (75) Inventor/Applicant (for US only): DAVIES, Raymond [GB/GB]; 9 Limpton Gate, Yarm, Cleveland TS15 9JA (GB). (74) Agents: GRATWICK, Christopher et al.; ICI Group Intellectual Property, P.O. Box 90, Wilton, Middlesbrough, Cleveland TS90 8JE (GB).		(81) Designated States: AU, BR, CA, CN, IN, JP, KR, NO, RU, US, European patent (AT, BE, CH, CY, DE, DK, ES, FI, FR, GB, GR, IE, IT, LU, MC, NL, PT, SE). Published <i>With international search report.</i>

(54) Title: CATALYST SUPPORT**(57) Abstract**

A catalyst support structure e.g. for use in an ammonia oxidation reactor, comprising a series of primary supports (19) disposed above a catalyst bed, a lattice assembly disposed beneath the catalyst bed and on which the catalyst bed rests, said lattice assembly being suspended from the primary supports (19) by suspending means (27) extending through the catalyst bed. Preferably the support structure includes a static start-up burner arrangement in the form of one or more perforated tubes (24) adjacent the primary supports (19).



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Catalyst support

This invention relates to a catalyst support and in particular to supporting catalysts for reactions effected at relatively high temperatures, especially in the manufacture of nitric acid by the oxidation of ammonia.

5 Heretofore in ammonia oxidation processes, the catalyst, often in the form of a stack or wad of wire gauzes or meshes of the active material, for example platinum, often in combination with other precious metals such as palladium, is supported on a lattice of steel beams disposed across the reaction vessel below the catalyst layer. Under conventional operating conditions, the reactants, e.g. a gaseous mixture of ammonia and air, are fed at an
10 elevated temperature, typically in the range 100 to 300°C, to the vessel space above the catalyst. On passage through the catalyst, the reaction takes place: being a strongly exothermic reaction, the gas temperature rapidly increases, typically to a temperature in the range 800 to 950°C. Consequently the support lattice is exposed to such high temperatures. The reaction vessel is typically 2 to 6 m in diameter and so in order to withstand the high
15 temperatures while supporting the catalyst without undue deformation, it has generally been necessary construct the lattice from relatively closely spaced steel beams of considerably depth, typically 15 to 30 cm, extending across the vessel. Such structures are heavy and, since they have to be constructed of materials that can withstand the harsh operating conditions, are expensive. Conventionally the lattice has been of a welded "bottle crate"
20 construction. Not only is such an arrangement heavy and expensive but it is prone to buckling and damage: being of welded construction renders repair difficult and expensive.

We have realised that much lighter, and hence cheaper and more easily handled, support structures can be employed if the primary support is from above the catalyst bed where the prevailing conditions are not so extreme.

25 Accordingly the present invention provides a structure for supporting a catalyst bed in a vessel comprising a series of primary supports extending across the vessel and a lattice assembly carrying the catalyst bed disposed beneath the primary supports and suspended therefrom via suspending means extending through the catalyst bed.

The invention is illustrated by reference to the accompanying drawings in which:

- 30 Figure 1 is a diagrammatic vertical section through an ammonia oxidation reactor,
 Figure 2 is a plan of the reactor with the upper shell member removed;
 Figure 3 is a section along the line III - III of Figure 2;
 Figure 4 is a plan of the base assembly of Figure 3 with the primary support member assembly and cover plate removed,
35 Figure 5 is an isometric sketch of part of the base assembly;
 Figure 6 is an enlarged plan of part of Figure 2 showing four of the base assemblies and the grid assembly supported thereby;

Figure 7 is an elevation of part of the grid assembly;

Figure 8 is a section along the line VIII - VIII of Figure 7 showing an adjacent grid assembly in broken lines;

5 Figure 9 is a section of part of the skirt illustrating the method of supporting the grid assembly at the walls of the vessel;

Figure 10 is a plan view of the arrangement of Figure 9;

Figure 11 is a view similar to the lower part of Figure 3 showing an alternative embodiment;

10 Figure 12 is a view similar to Figure 10 illustrating the method of supporting the grid assembly at the walls of the vessel for the alternative embodiment;

Figure 13 is a view similar to that of Figure 8 showing the alternative embodiment;

Figure 14 is a view similar to Figure 3 showing an alternative start-up burner arrangement;

Figure 15 is a view similar to Figure 14 showing another start-up burner arrangement.

15 Referring to Figure 1 an ammonia oxidation reactor consists of an outer shell of generally circular cross section formed as upper and lower shell members 10, 11, provided with a reactants inlet port 12 and a reaction products outlet port 13 respectively. The upper shell member is provided with a perforate diffuser plate 14 extending across the shell. The diameter of the reactor is typically about 4 m.

20 The lower shell member carries a skirt 15 located round the interior periphery of the vessel by means of an outwardly extending flange resting in a rebate 16 in the upper rim of the lower shell member 11. Skirt 15 has an upper cylindrical portion and then an inwardly tapered, i.e. frusto-conical, portion 17. Since, in operation the lower portion of the skirt is liable to be at a much higher temperature, e.g. about 900°C, than the upper portion which is typically at about
25 300°C, the conical configuration permits some differential thermal expansion of the lower portion of the skirt relative to the upper portion.

As shown in Figure 2, a number of channel sectioned supports 18 are welded to the upper part of the conical portion of the skirt in chordally disposed pairs. Typically there are five pairs of supports 18. Each pair of channel section supports carries a primary support
30 member 19. These primary support members carry a lattice assembly: since the primary support members are located above the catalyst bed, they are disposed in the relatively cool part of the reactor and so do not need to be made from a material that can withstand the high temperatures encountered in or below the catalyst bed. The primary support members may be solid or hollow and may be of any convenient cross section. However they are preferably
35 pipes, since pipes of suitable material and size are readily available. The number, configuration and size of the primary support members required will depend on the size of the reactor and the load to be supported. Typically with a reactor diameter of 4 m, there may be

used five primary support members in the form of pipes of diameter about 10 cm spaced at about 80 cm intervals.

The lattice assembly comprises a plurality of base assemblies 20 connected by pairs of grid supports 21 and a plurality of grid assemblies 22 (only one of which is shown in Figure 2) carried by the grid supports 21. As described hereinafter, the grid supports 21 are attached to the lower frusto-conical configuration portion 17 of the skirt member 15.

A number of base assemblies 20 are suspended from each primary support member 19. Typically these assemblies are disposed in a square configuration at a pitch corresponding to the spacing of the primary support members 19. The catalyst bed (shown by the dotted line 23 in Figure 1 and only shown in part in Figure 2) is disposed on top of the base and grid assemblies. Although preferred, it is not necessary that the base assemblies 20 are disposed in a square pattern: thus they may be disposed in other configurations, e.g. rectangular or triangular patterns.

Although the base and grid assemblies are located in the high temperature region of the reactor, the loads borne by the individual assemblies are relatively low. In particular there are no individual load bearing members extending across the whole span of the reactor in the high temperature region and so massive construction to withstand large deformation loads is not necessary. Consequently the mass of high temperature resistant materials is reduced.

Whereas in a conventional ammonia oxidation reactor, the reaction is initiated by heating the catalyst bed by means of a rotating burner directing a flame obtained by combusting a combustible gas e.g. hydrogen on to the catalyst bed, such a construction is not suitable in the present invention as any such burner would need to be disposed above the primary support members and so subject them to localised high temperatures during start-up.

In the present invention this problem is overcome by providing a static start-up burner arrangement in the form of one or more tubes adjacent the primary support members and means to supply a combustible gas thereto. The tube, or tubes, is provided with perforations (not shown) at intervals so that a flame can be directed down and, preferably, outwards from the tube on to the catalyst bed. As shown in Figures 1, 2 and 3, the start-up burner may comprise a single serpentine tube 24 adjacent the primary support members 19. For clarity, in Figure 2, this serpentine tube is shown part in full and part by dotted lines. A fuel gas, for example hydrogen, may be fed to the serpentine tube 24 through a suitable inlet pipe 25 shown dotted in Figure 2.

Referring to Figures 2 and 3, the serpentine tube 24 is supported on brackets 26 located at each secondary assembly suspension point. For clarity in Figure 2, the brackets 26 are shown only at the locations where serpentine tube 24 is shown by full lines. As shown in Figure 3, the brackets 26 and the base assemblies 20 are supported from primary support members 19 by tie rods 27. Although these tie rods are load bearing and subject to high

temperatures at their lower ends, they are in tension and so not subject to buckling loads. To permit adjustment during assembly of the whole catalyst support structure, the location of the base assemblies 20 relative to the primary support members 19 is preferably by means of threaded portions and nuts at the upper and/or the lower ends of the tie rods 27.

5 The base assemblies 20 are shown in more detail in Figures 3, 4 and 5. Supported by each tie rod 27 is a base member 28, which is preferably a casting to avoid the need for welds, and a cover plate 29. Where the base assemblies 20 are disposed in a square or rectangular configuration, each base member 28 is preferably of octagonal configuration and has inner and outer upstands 30, 31, arranged in pairs. For a square or rectangular configuration of base
10 assemblies 20, each base member 28 has four pairs of upstands.

Each outer upstand 31 is provided with a slot 32 through its wall. The inner and outer upstands are provided with two pairs of notches 33 in their upper surface (see Figure 5). Located in each pair of notches 33 is a hinge member 34 having rounded projections 35
15 engaging with the notches. Each hinge member 34 is thus able to pivot relative to the inner and outer upstands. When assembled, the cover plate 29 of the base assembly 20 acts as a keeper to retain the projections 35 of hinge members 34 in the notches 33 of the upstands.

Each hinge member 34 is also provided with a pin 36, positioned at a location below the axis of projections 35, projecting from the hinge member 34 in a direction perpendicular to the axis of the rounded projections 35. A grid support 21 having an elongated slot 37 at each
20 end is mounted on each pin 36 and extends through the slot 32 in the outer upstand 31. The grid support is thus supported by a pin 36 on a hinge member 34 pivoting in the base member 28 about an axis parallel to, but above, said pin. The grid supports 21 thus extend from the base member 28 in a direction parallel to the axis of the rounded projections 35. Each grid support 21 engages at its other end with a corresponding pin on a hinge member of an
25 adjacent base assembly or with a pin connected to the periphery of the lower portion 17 of the skirt 15. The mounting of the grid supports at the periphery of the skirt is described hereinafter with reference to Figure 9.

By virtue of the elongated slots 37, the grid supports 21 are free to move longitudinally with respect to the base members 28, and by virtue of the hinge members 34, are also free to
30 swing laterally to permit displacement of the grid supports 21 in the lateral direction. Since each pair of notches 33 in the upstands 30, 31 carries a hinge member 34 and each hinge member 34 carries a grid support 21, the base assemblies 20 are connected by pairs of grid supports 21 spaced apart from one another and free to move laterally and longitudinally relative to one another. The base assemblies 20, and hence tie rods 27, are thus not subjected to
35 thermally induced lateral stresses and so forces tending to give rise to buckling are minimised.

Referring to Figure 6, where four adjacent base assemblies 20 are shown connected by pairs of grid supports 21. A grid assembly 22 is shown located on the inner grid support of

each pair. The grid assembly comprises an outer octagonal ring member 38 dimensioned such that it can expand through thermal expansion without imposing undue forces on adjacent grid assemblies on the other grid supports of the grid support pairs and on the base assemblies 20. To avoid welds, the ring 38 may be simply be of bent metal construction. Ring member 38 is provided with downwardly extending locating lugs 40 which serve to position the grid assembly relative to the grid supports 21. Expansion of ring 38 thus causes the grid supports 21 to move longitudinally and laterally but, as previously described, because of the mounting of the grid supports 21 via hinge members 34 and elongated slots 37 in the ends of the grid supports 21, such longitudinal and lateral movement does not give rise to buckling forces on the base assemblies 20 and tie rods 27.

As shown in Figures 6, 7 and 8, the opposed sides of the ring member 38 are provided with a plurality of notches in the upper surface: The notches 41 in one pair of opposed sides serve to support rebated cross bars 42 which in turn have notches 43 which support rods 44. The ends of rods 44 are located in notches 45 in the other pair of opposed sides of ring member 38. The upper surfaces of the cross bars 42, rods 44, and ring 38 are preferably substantially co-planar with the upper surface of the cover plates 29. The notches, rebates on bars 42, and the lengths of the bars and rods are dimensioned such that relative movement is possible to accommodate thermal expansion. The number and spacing of the rods and bars will depend on the tolerable "sag" of the catalyst layer disposed above the grid assemblies. Generally, as hereinafter described, a wire mesh 46 is disposed on top of the grid assemblies to act as a support between adjacent cross bars and rods. Typically the spacing between adjacent cross bars and between adjacent rods is in the range 2 to 15 cm, particularly in the range 3 to 12 cm. It will be appreciated that it is not necessary that the spacing between adjacent cross bars 42 is the same as the spacing between adjacent rods 44.

In Figures 9 and 10, the mounting of the grid supports 21 at the periphery of the skirt is shown. In Figure 10, the mesh 46 is omitted for clarity. At the requisite locations, brackets 47 are welded to the lower conical portion 17 of the skirt. A pair of hinge members 48 are pivoted in each bracket about an axis parallel to the length of the grid supports 21 by means of hinge pins 49. Each hinge member 48 has a pin 50 extending laterally from the hinge member but displaced vertically from the hinge pin 49. Each pin 50 engages with the elongated slot 37 in the end of the associated grid support 21. It will be appreciated that the ring members adjacent the periphery of the skirt will be shaped to conform to the areas enclosed by the skirt and the grip supports 21.

By arranging that the hinge members 34, 48 are pivoted at a location above the pins 36, 50 supporting the grid supports 21, the grid supports 21 will tend to be in their lowest position when the assembly is assembled at ambient temperature and differential thermal expansion will cause pivoting of the hinge members 34, 48 with consequent lateral movement

accompanied by slight raising of the grid supports 21. On cooling and contraction of the assembly, the hinge members will thus tend to revert towards their lowest position.

In an alternative embodiment, as shown in Figures 11, 12 and 13, a simpler construction may be employed, omitting the hinge members. In this embodiment, each grid support 21 has a projecting notched lug 51 at each end which engages in an elongated slot or notch 52 in the outer upstand 31 of the base member 28 and the inner upstand is omitted. Similarly at the periphery of the skirt, the lugs 51 engage with slots or notches 53 in the brackets 47 fastened to the lower portion 17 of the skirt. The grid supports 21 are thus free to expand longitudinally and to move laterally in the slots 52 and 53. In this embodiment the octagonal ring member is omitted and the cross bars 42 are mounted in notches 54 in the upper surface of the grid supports 36. The ends of the cross bars 42 are provided with notches 55 which engage with the notches 54 in the grid supports. On thermal expansion or contraction of the cross bars 42, the grid supports 21 are thus moved laterally in slots or notches 52, 53. By virtue of the notches 55, on contraction on cooling, the grid supports tend to return to their cold, undisplaced position.

It will be appreciated that the whole supporting assembly can be constructed simply by supporting the base members 28 (having the tie rods 27 extending upwardly therefrom) and skirt 15 (having its channel section supports 18 and flanges 47 welded or otherwise fastened thereto) on a suitable substrate: the grid supports 21 (and, if used, hinge members 34, 48) are then located on the base members 28 and flanges 47. The octagonal rings 38 (if used) are then positioned on the grid supports 21 and cross bars 42 located in the appropriate notches 41 or 54. The rods 44 are then positioned in the notches 43 in the cross bars 42, cover plates 29 positioned and then the wire mesh 46, having holes at intervals for the tie rods 27, is laid over the rods 44 and cover plates 29. The wire mesh, preferably in a single piece, extends all over the area of the skirt and may be fastened to the periphery thereof, e.g. by welds, if desired. The catalyst, which may be a wad of wire gauzes or particulate, is then disposed above the mesh 46. The brackets 26, serpentine tube 24 and primary support members 19 are then positioned on the tie rods 27 with the primary support members 19 resting in the channel section supports 18. A nut 56 (See Figure 3) is then applied to the upper end of each tie rod 27. The skirt 15 carrying the whole assembly can then be lifted and placed in the reactor.

In the embodiment described above, the catalyst bed is heated to the ignition temperature by combusting a gas supplied via the serpentine tube 24. While this allows all of the bed to be heated simultaneously, this arrangement may present practical difficulties in view of the relatively large amount of fuel gas, e.g. hydrogen required. An alternative arrangement is to heat the sections of the bed in turn. This may be achieved by replacing the serpentine tube by a number of separate tubes parallel with each primary support member with means to

isolate each tube from the gas supply except when it is desired to heat the section of the catalyst bed below that tube.

In another arrangement the primary support members may be disposed radially, instead of parallel to one another, thus providing sectors of the lattice assembly that are free from tie rods. In this case the primary support members may be displaced vertically relative to one another so that they cross over one another at the centre of the apparatus. In this way the need for a welded junction member at the centre can be avoided. The start-up heater can then be in the form of a plurality of radially extending burner tubes having a plurality of perforations disposed so that a flame can be directed down from the tube or tubes on to the catalyst bed, and means are provided to oscillate the radially extending burner tubes about the longitudinal axis of the apparatus below the primary support members across the sectors between the tie rods. The radially extending burner tubes are supplied with the fuel gas from a central supply pipe.

Alternative, preferred, start-up burner arrangements are shown in the embodiments of Figures 14 and 15. In the arrangement of Figure 14, which is a view similar to that of Figure 3 with the base assembly 20 shown dotted, the serpentine tube 24 and its support brackets 26 are omitted and the tie rods 27 are hollow for part of their length. Radial holes 57 are bored at a suitable location above the catalyst bed to communicate with the hollow interior 58 of the tie rods 27 and so provide burner orifices. To effect start-up, a fuel gas, e.g. hydrogen, is supplied to the upper end of the hollow interior 58 of the tie rod by means not shown and flows down through the hollow interior of the tie rod and emerges through the burner orifices where it combusts to provide a flame to heat the catalyst bed.

It will be appreciated that the tie rod may be a tube with a suitable cap or plug at its lower end. Alternatively each tie rod may be constructed in sections; for example a solid rod lower section and an upper tubular section and these may be welded or screw-threaded together.

In the arrangement of Figure 15, which is similar to Figure 14 but showing just the upper part of the tie rod assembly, each tie rod is provided, above the catalyst bed, with a burner assembly in the form of an enclosure in the form of a hollow cylindrical casing 59 provided with perforations 60 at suitable locations to form burner orifices and a fuel gas feed tube 61.

It will be appreciated that in the arrangements of Figures 14 and 15, the burner orifices may be inclined to direct the flame down on to the catalyst bed if desired. Where the base assemblies 20 and tie rods 27 are disposed in a square configuration, as in Figure 2, each tie rod may be provided with four burner orifices directed towards the tie rod that is disposed diagonally opposite in the aforesaid square configuration. It will also be appreciated that in some cases it may not be necessary to provide each tie rod with a burner arrangement: for

example alternate tie rods may be so provided. A suitable igniter, e.g. a spark plug, (not shown), may be provided to effect ignition of the fuel. Since the flame can propagate from one burner to another, it is not necessary to provide each burner with such ignition means.

5 The catalyst may be, as mentioned above, a wad of meshes or gauzes of a precious metal, e.g. platinum alloyed with rhodium, or alternatively may be a fixed bed of a particulate catalyst for example a rare earth/cobalt oxides composition as described in our WO 98/28073.

Claims.

1. A structure for supporting a catalyst bed in a vessel comprising a series of primary supports extending across the vessel and a lattice assembly carrying the catalyst bed disposed beneath the primary supports and suspended therefrom via suspending means extending through the catalyst bed.
2. A structure according to claim 1 wherein the primary supports extend chordally across the vessel.
3. A structure according to claim 1 or claim 2 wherein the lattice assembly comprises a plurality of secondary support assemblies and a plurality of grid assemblies carried by the secondary support assemblies.
4. A structure according to claim 3 wherein a number of secondary support assemblies are suspended from each primary support by tie rods.
5. A structure according to claim 4 wherein the secondary support assemblies are disposed in a square configuration.
6. A structure according to claim 4 or claim 5 wherein the secondary support assemblies comprises base members connected by of pairs of grid supports supported by the base members and capable of longitudinal and lateral movement relative to one another and relative to the base members.
7. A structure according to claim 6 the grid supports are supported by pins to hinge members pivoting in the base members about an axis parallel to, but above, said pins.
8. A structure according to claim 6 or claim 7 wherein a grid assembly is supported by the inner one of each pair of grid supports connecting adjacent base members.
9. A structure according to claim 8 wherein the grid assembly comprises members extending across the area enclosed by said inner grid supports but free to move longitudinally relative thereto.
10. A structure according to claim 9 wherein said grid assembly includes a ring member engaging with said inner grid supports, and said members extending across the area

enclosed by said inner grid supports are located in notched in the upper surface of said ring member.

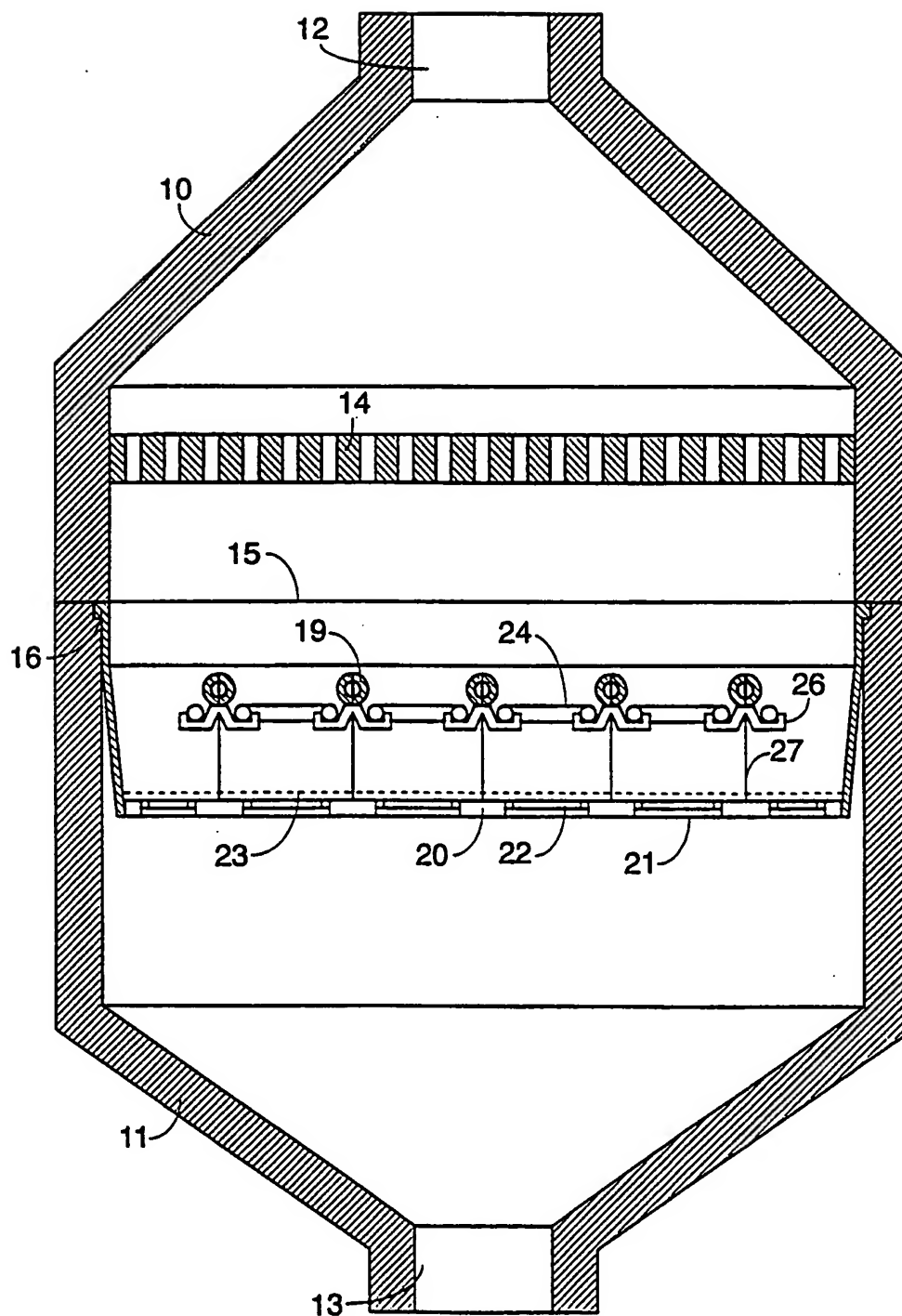
11. A structure according to any one of claims 1 to 9 for use for the oxidation of ammonia wherein the catalyst bed comprises a wad of gauzes or meshes of a precious metal.
12. A structure according to any one of claims 1 to 9 for use for the oxidation of ammonia wherein the catalyst bed comprises a fixed bed of particles of a rare earth/cobalt oxides composition.
13. A structure according to claim 1 wherein the primary support members are disposed radially.
14. A structure according to any one of claims 1 to 13 including a static start-up burner arrangement in the form of one or more perforate tubes adjacent the primary supports and means to supply a combustible gas to said tube or tubes, the perforations in said tube or tubes being disposed so that a flame can be directed down from the tube or tubes on to the catalyst bed.
15. A structure according to claim 14 wherein said start-up burner comprises a single perforate tube disposed adjacent the primary supports in a serpentine configuration.
16. A structure according to any one of claims 1 to 13 wherein the suspending means comprises tie rods and at least some of which are provided with a start-up burner arrangement.
17. A structure according to claim 16 wherein at least some of the tie rods are hollow and have radial holes therein and means are provided to supply a fuel gas to the interior of said hollow tie rods.
18. A structure according to claim 16 wherein at least some of the tie rods are provided with an enclosure surrounding the tie rod for at least part of its length, said enclosure being provided with burner orifices and means to supply a fuel gas to said enclosure.
19. A structure according to claim 13 including a start-up burner arrangement in the form of a plurality of radially extending burner tubes one for each sector, each tube having a plurality of perforations disposed so that a flame can be directed down from the tube or

tubes on to the catalyst bed, and means are provided to oscillate the radially extending burner tubes about the longitudinal axis of the apparatus below the primary support members.

20. A structure according to any one of claims 1 to 19 wherein said primary supports are carried by a skirt member located round the interior periphery of the vessel.
21. A structure according to claim 20 wherein the lower portion of the skirt member is of frusto-conical configuration, and the lattice assembly is attached at intervals to said lower portion.

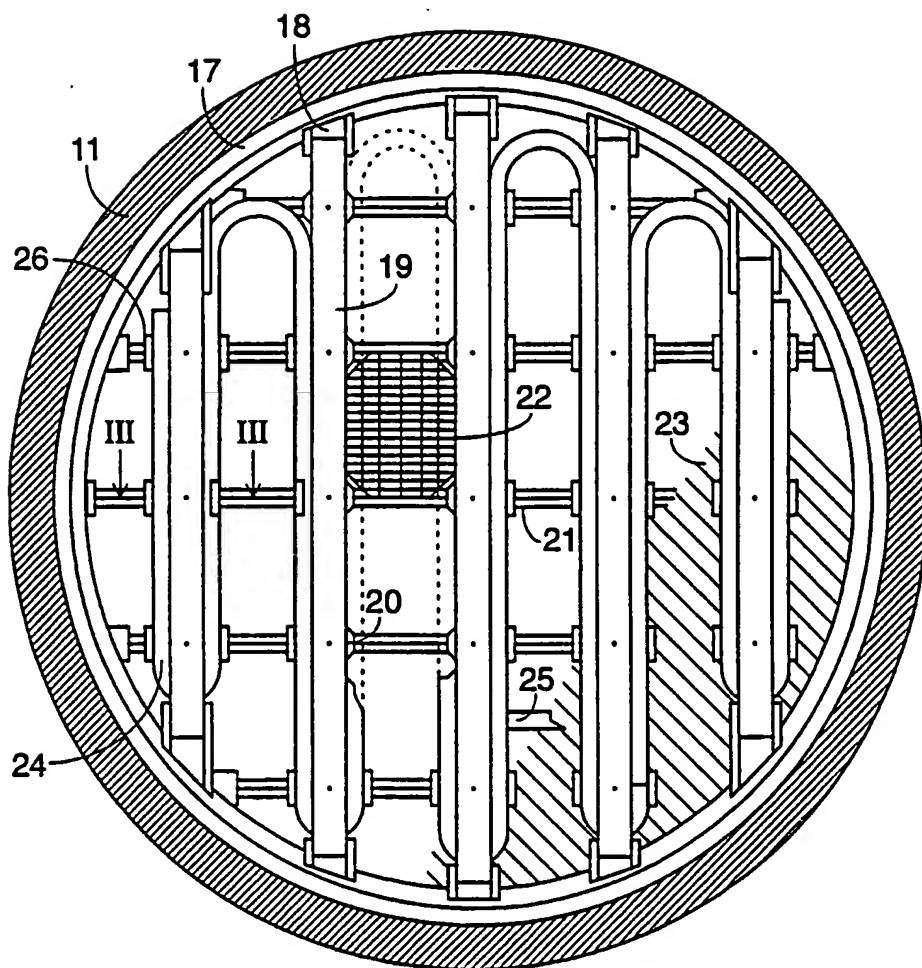
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Fig.1.



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Fig.2.



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Fig.3.

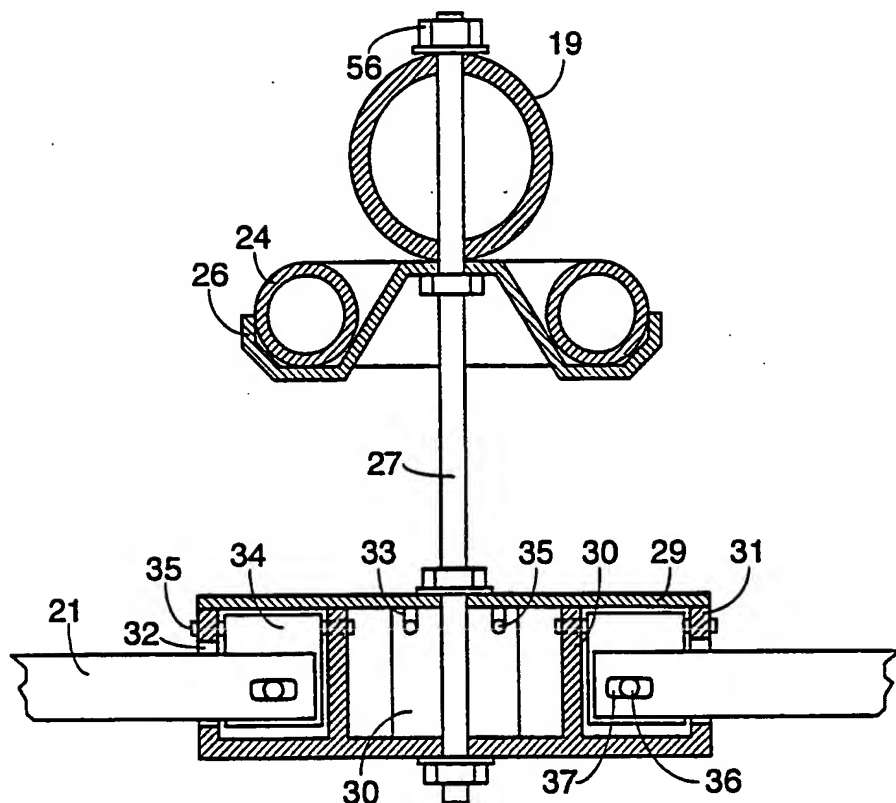
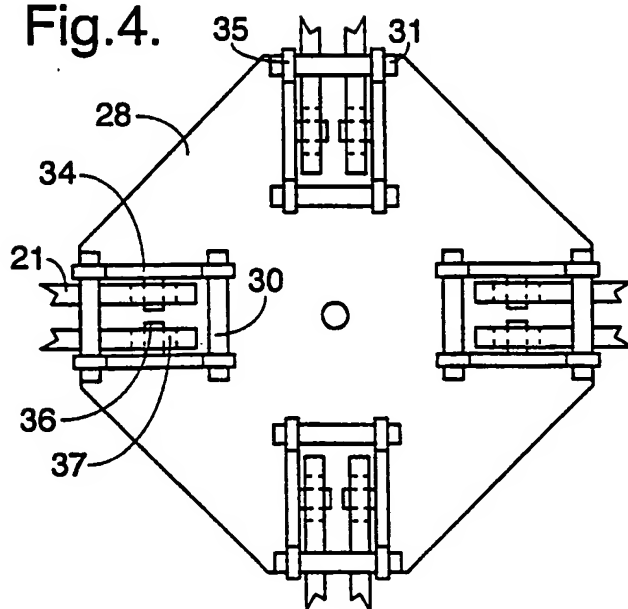


Fig.4.



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Fig.5.

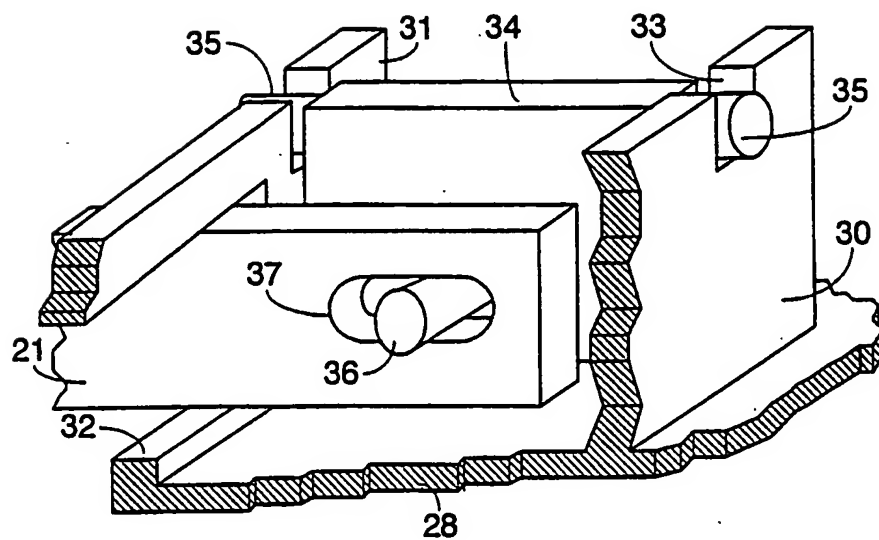
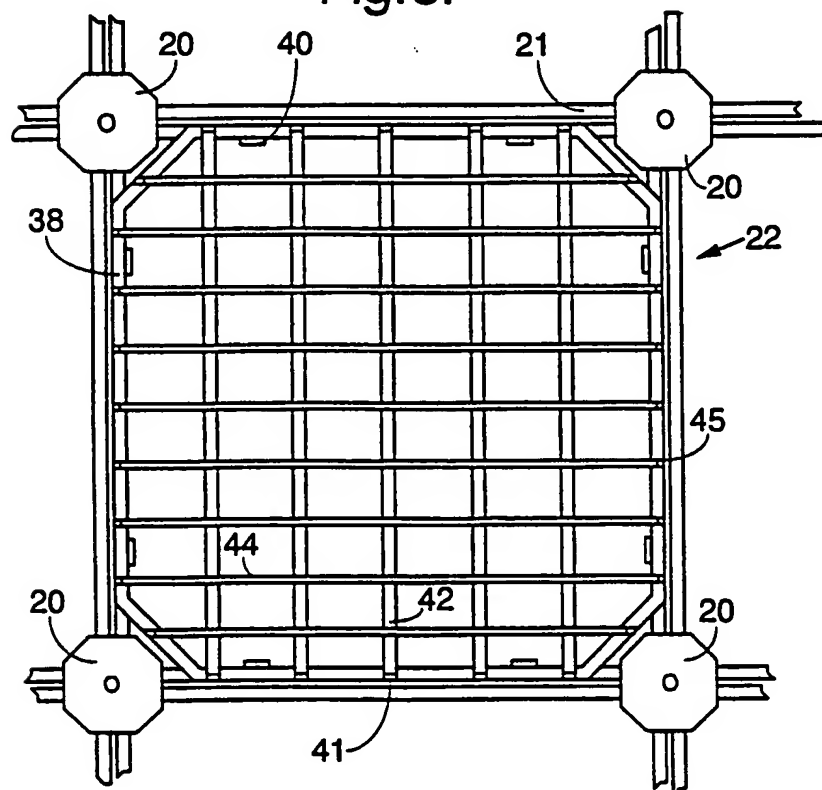


Fig.6.



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Fig.7.

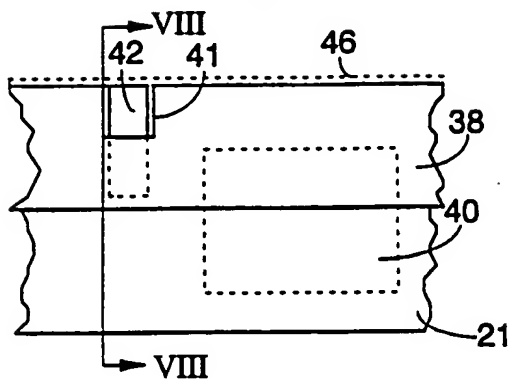


Fig.8.

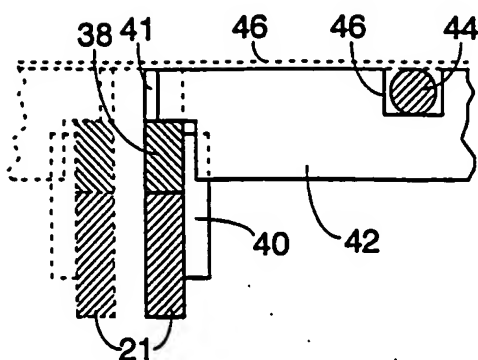


Fig.9.

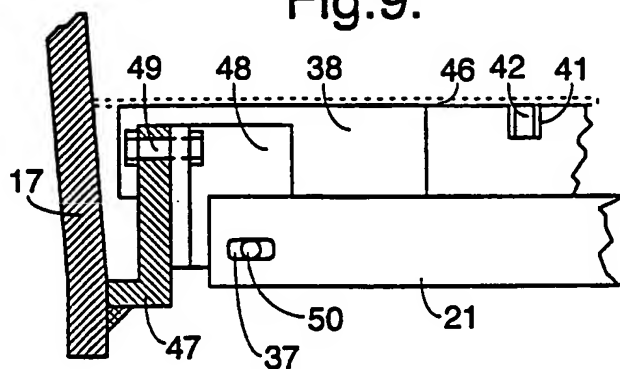
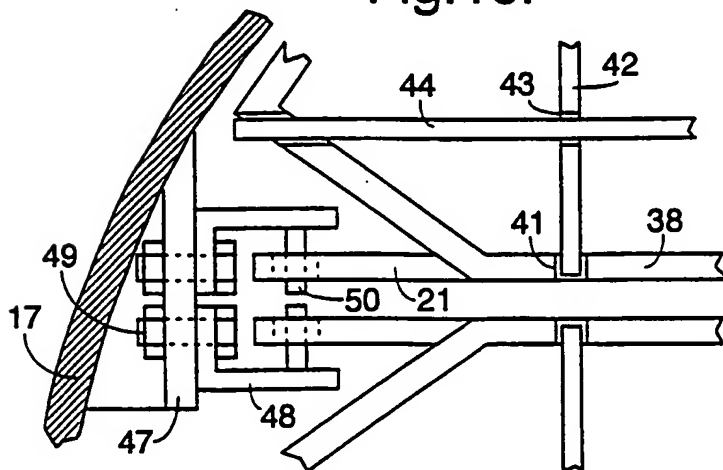


Fig.10.



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Fig.11.

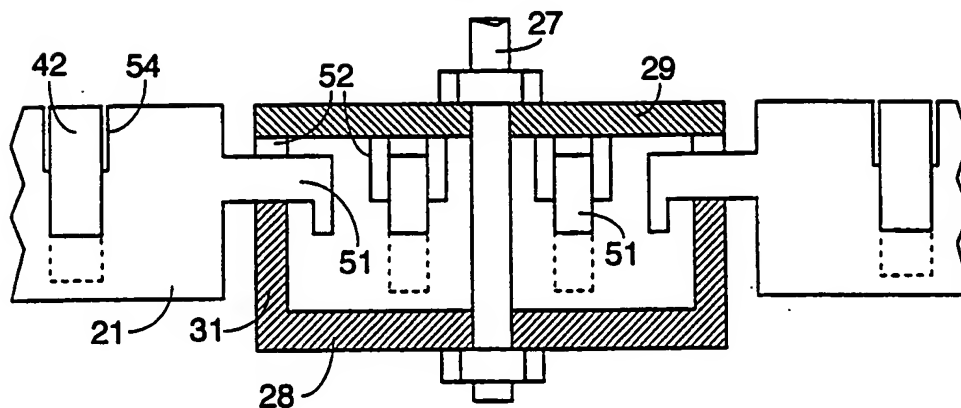


Fig.12.

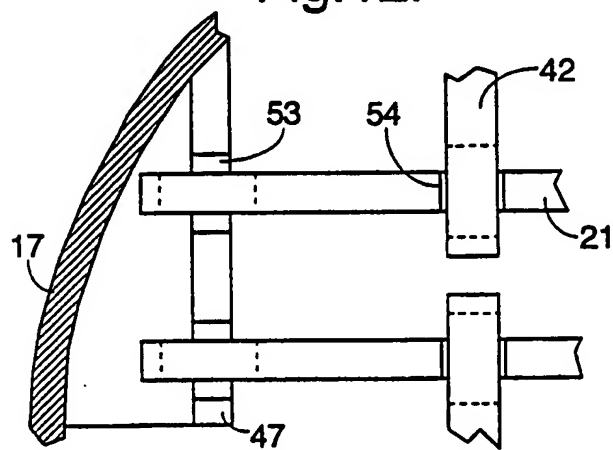
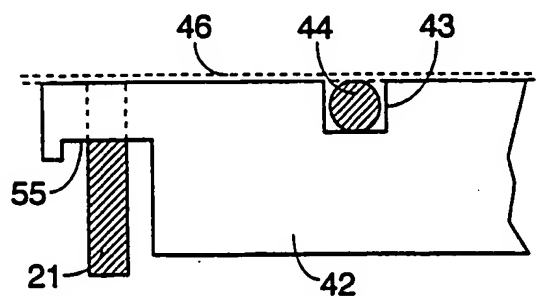


Fig.13.



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Fig.14.

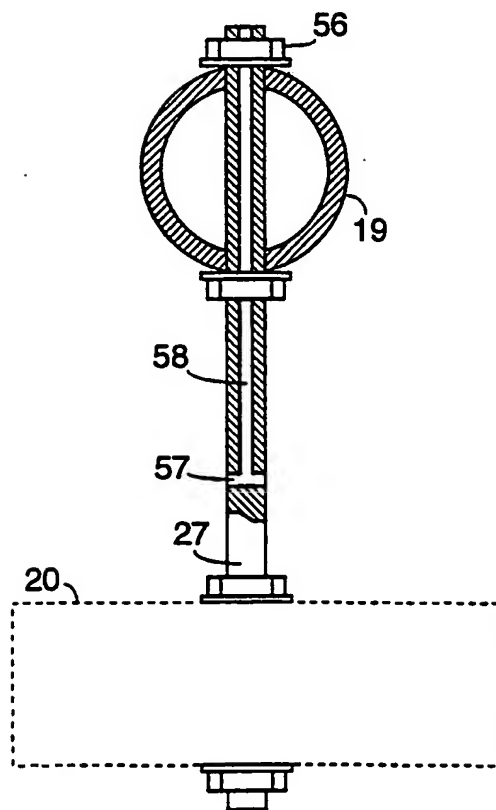
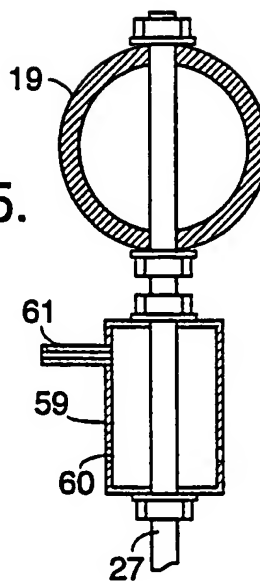


Fig.15.



INTERNATIONAL SEARCH REPORT

Intern. Appl. No.

PCT/GB 99/04188

A. CLASSIFICATION OF SUBJECT MATTER

IPC 7 B01J8/02 B01J8/00 C01B21/26 C01B21/28

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC 7 B01J C01B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the International search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 3 482 946 A (SHIRK ROBERT M) 9 December 1969 (1969-12-09) column 3, line 16 - line 50 claims 1-7; figures 1-5 ---	1-4, 14, 15, 20
A	US 4 195 064 A (BETTEKEN JOSEPH C ET AL) 25 March 1980 (1980-03-25) column 5, line 60 - column 8, line 37 claims 1-7; figures 5-10 ---	1, 3-6
A	FR 2 253 554 A (BRITISH PETROLEUM CO) 4 July 1975 (1975-07-04) page 5, line 33 - page 7, line 15 figures 1-4 ---	1, 14
A	DE 37 31 988 A (STEINMUELLER GMBH L & C) 6 April 1989 (1989-04-06) the whole document -----	11, 12



Further documents are listed in the continuation of box C.



Patent family members are listed in annex.

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Date of the actual completion of the international search

21 March 2000

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INTERNATIONAL SEARCH REPORT

Information on patent family members

Inter. Patent Application No

PCT/GB 99/04188

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